

# CORRIGENDUM TO “ESTIMATING WEPP CROPLAND ERODIBILITY VALUES FROM SOIL PROPERTIES”

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## HIGHLIGHTS

- Interrill erodibility  $K_i$  values presented in Elliot and Flanagan (2023) were incorrect, and correct values are given.
- Interrill erodibility can be estimated from a soil's sand, very fine sand, and clay contents.

**ABSTRACT.** In Elliot and Flanagan (2023), the interrill and rill soil erodibility of 36 cropland soils was reported, along with correlations among soil erodibility and other soil properties, and equations to estimate erodibility from readily measured soil properties. Early versions of the Water Erosion Prediction Project (WEPP) model had linked interrill detachment rate to the square of the rainfall intensity and an interrill soil erodibility constant  $K_{i1}$ . By the time the WEPP model was released for general use in 1995, the developers had changed the interrill detachment rate to be a function of the product of rainfall intensity and runoff and a different interrill erodibility constant,  $K_{i2}$ . The interrill erodibilities ( $K_{i2}$ ) with this altered relationship were not the same as  $K_{i1}$  values developed to support earlier releases of the WEPP model. The authors, when reviewing some of the past literature supporting Elliot and Flanagan (2023), had mistakenly reported  $K_{i2}$  values when the numbers reported were in fact  $K_{i1}$  values. A closer examination of the entire data set and the identification of a published source for the correct  $K_{i2}$  values confirmed this mistake. This corrigendum reports the corrected  $K_{i2}$  values, the correlation of those revised values with other soil properties, and confirmation of a 1995 regression equation relating  $K_{i2}$  to three readily measured soil properties: sand content, very fine sand content, and clay content. The coefficient of determination for the 1995 regression equation was 0.80. We recommend that all references to  $K_{i2}$  in Elliot and Flanagan (2023) be changed to  $K_{i1}$  except the discussion about the findings of Mirzaee and Ghorbani-Dashtaki (2021), discussion about  $K_{i2}$  in Alberts et al. (1995), and equations 2 and A16. A marked up copy of Elliot and Flanagan (2023) showing these changes can be downloaded from [https://www.fs.usda.gov/rm/pubs\\_journals/2023/rmrs\\_2023\\_elliot\\_w001\\_corr.pdf](https://www.fs.usda.gov/rm/pubs_journals/2023/rmrs_2023_elliot_w001_corr.pdf).

**Keywords.** Cropland Soils, Interrill Erodibility, Water Erosion Prediction Project.

## BACKGROUND

After publishing “Estimating WEPP Cropland Erodibility Values from Soil Properties” (Elliot and Flanagan, 2023), the authors discovered that they had not used the correct values for the current interrill erodibility  $K_{i2}$  required by the WEPP Model. The purpose of this corrigendum is to present the correct  $K_i$  values now required by the WEPP model, show the relationships between the  $K_{i2}$  values and other soil

properties, and confirm a simplified regression model to estimate  $K_{i2}$  from measurable soil properties.

Elliot and Flanagan (2023) presented two interrill erosion models that had been applied in the development of the Water Erosion Prediction Project (WEPP) model. In the earliest versions of the WEPP model in 1987 until about 1993, interrill detachment was estimated by:

$$D_i = V S_f K_{i1} I^2 \quad (1)$$

where

$D_i$  = interrill detachment rate ( $\text{kg m}^{-2} \text{s}^{-1}$ )

$V$  = vegetation factors

$S_f$  = slope factor

$K_{i1}$  = interrill erodibility for equation 1 ( $\text{kg s m}^{-4}$ )

$I$  = rainfall intensity ( $\text{m s}^{-1}$ ).

When the WEPP model was recoded between 1993 and 1995, the interrill detachment model was altered to:

$$D_i = V S_f K_{i2} I q \quad (2)$$

where

$K_{i2}$  = interrill erodibility for equation 2 ( $\text{kg s m}^{-4}$ )

$q$  = runoff rate ( $\text{m s}^{-1}$ ).

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Elliot and Flanagan (2023) described the field study in detail from which  $K_{i1}$  and  $K_{i2}$  were derived. Following discussions with colleagues and a closer examination of the values for  $K_{i1}$  and  $K_{i2}$  in Elliot and Flanagan (2023), we determined that all the cited works from earlier proceedings and published papers in Elliot and Flanagan (2023) were in fact  $K_{i1}$ . Values for  $K_{i2}$  were categorized by texture in Alberts et al. (1995), but not published for individual soils. Recently, the authors found that values for  $K_{i2}$  were reported in the Huffman et al. (2013) textbook as well as the Fifth edition (Fangmeier et al., 2006) and Sixth edition (Huffman et al., 2011) of that textbook. This corrigendum presents the  $K_{i2}$  values from Huffman et al. (2013), the correlation coefficients of those values with other erodibility values and soil properties and confirms the accuracy of the predictive equations from Alberts et al. (1995) to estimate  $K_{i2}$  from readily measured soil properties. In this corrigendum, we report the last published values for  $K_{i1}$  from the literature cited in Elliot and Flanagan (2023), and  $K_{i2}$  values from Huffman et al. (2013). We used an Excel spreadsheet to recalculate all the correlation coefficients between  $K_{i1}$ ,  $K_{i2}$ , and other soil properties. All equations, tables, and discussion in Elliot and Flanagan (2023) about interrill erodibility should be read as  $K_{i1}$  except equations 2 and A16, the references about  $K_{i2}$  in Alberts et al. (1995), and the findings of Mirzaee and Ghorbani-Dashtaki (2021). These changes have been noted in a marked-up copy of Elliot and Flanagan (2023) that can be downloaded from [https://www.fs.usda.gov/rm/pubs\\_journals/2023/rmrs\\_2023\\_elliot\\_w001\\_corr.pdf](https://www.fs.usda.gov/rm/pubs_journals/2023/rmrs_2023_elliot_w001_corr.pdf).

## RESULTS

Table 1c is similar to table 1 in Elliot and Flanagan (2023), except some  $K_{i1}$  and all  $K_{i2}$  values were changed and are shown in bold. On average,  $K_{i2}$  was nearly double the value of  $K_{i1}$ .  $K_{i2}$  values for coarse-textured soils with lower runoff rates were remarkably greater than  $K_{i1}$ , note soil numbers 24 and 25. Also, soils with a high very fine sand content had a much greater  $K_{i2}$  value compared to  $K_{i1}$ , like soil numbers 5, 8, and 32. Huffman et al. (2013) did not have a  $K_{i2}$  value for soil 3. We observed that the observed value for  $K_{i2}$  for soil 6 was much lower than similar silt loam soils, likely due to the high root content as described in Elliot and Flanagan (2023), so we did not include this soil in the subsequent statistical analyses.

The correlation coefficients were recalculated for both  $K_{i1}$  and  $K_{i2}$  and are presented in table 5c. Correlation between  $K_{i1}$  and  $K_{i2}$  was weak ( $r = 0.39$ ). The highest correlation for  $K_{i2}$  was with the very fine sand content  $VfSa$  ( $r = 0.59$ ). The soil classification order that was highly correlated with  $K_{i1}$  ( $r = 0.52$ ) was not correlated with  $K_{i2}$  ( $r = 0.07$ ). The saturated base hydraulic conductivity  $K_b$  has been added in table 5c as it related to runoff, and it was weakly correlated with  $K_{i2}$  ( $r = 0.29$ ).

With the corrected values for  $K_{i2}$ , we could not improve on the  $K_{i2}$  predictive equation that was originally proposed in Alberts et al. (1995) for estimating  $K_{i2}$  using limited soil properties:

$$\begin{aligned} \text{For Sand} \geq 30\% \quad K_{i2} &= 2.7 + 0.19 VfSa \quad \text{and} \\ \text{For Sand} < 30\% \quad K_{i2} &= 6.05 - 0.055 Clay \quad r^2 = 0.80 \end{aligned} \quad (12c)$$

where

$K_{i2}$  = interrill erodibility  $\times 10^{-6}$  ( $\text{kg s m}^{-4}$ )

$Sand$  = Sand content (0.05 mm – 2 mm dia) of fine fraction (<2 mm dia) (percent)

$VfSa$  = Very fine sand content (0.05 mm – 0.01 mm dia) of fine fraction (<2 mm dia) (percent)

$Clay$  = Clay content (<0.002 mm dia) of fine fraction (<2 mm dia) (percent).

Figure 4c shows the predicted  $K_{i2}$  values from equation 12c vs. the updated observed values and one observation from an independent study by Mirzaee & Ghorbani-Dashtaki (2021).

## DISCUSSION

The  $K_{i2}$  values were originally derived by Laflen in the mid-1990s from the Elliot et al. (1989) field data but were not published until 2006 in Fangmeier et al. (2006). The  $K_{i1}$  estimates were made from the last two to four samples collected from the interrill erosion plots recorded in Elliot et al. (1989) when runoff had reached “equilibrium,” but Laflen used more points to estimate  $K_{i2}$  as equation 2 considered runoff rate as well as rainfall intensity. How many of those points Laflen used is not known, so there is scope to recalculate  $K_{i2}$  from the data in Elliot et al. (1989) and quantify the effect of the analytical methods on determining  $K_{i2}$ .

Table 5c shows that the revised  $K_{i2}$  values were poorly correlated with the  $K_{i1}$  values ( $r = 0.39$ ). However, correlation between  $K_{i2}$  and very fine sand was exceptionally high (table 5c;  $r = 0.59$ ). The correlation with the soil classification order that was high with  $K_{i1}$  ( $r = 0.52$ ) was weak with  $K_{i2}$  ( $r = 0.07$ ). Table 1c shows that  $K_{i1}$  and  $K_{i2}$  values tended to differ the most on soils that were high in sand content where observed runoff rates were low (soil numbers 24 and 25), or soils high in very fine sand where  $K_{i2}$  values were high (soil numbers 5 and 8). The correlation of  $K_{i2}$  with saturated hydraulic conductivity ( $r = 0.29$ ) was not as great as many of the other variables in table 5c that were related to soil texture.

The predictive equation originally proposed by Alberts et al. (1995) considered both sand and very fine sand in the prediction. The coefficient of determination for the simplified predictive equation 12c from Alberts et al. (1995) was greater for  $K_{i2}$  ( $r^2 = 0.80$ ) than for  $K_r$  ( $r^2 = 0.73$ ) or  $\tau_c$  ( $r^2 = 0.62$ ) in Elliot and Flanagan (2023).

Of the four outlier points in figure 4c, the overestimation of the Mirzaee and Ghorbani-Dashtaki (2021) was likely due to differences in field methods as discussed in Elliot and Flanagan (2023). Two of the other three overpredictions were Soil 1 (Brenneman, 1988) and Soil 10, which, like soil 6, had not been in fallow the year prior to the experiment, and thus roots in the soil may have reduced the measured interrill erodibility.

**Table 1c. Site number, soil series, location, erodibility, and textural properties of WEPP cropland soils with corrected values for  $K_{t1}$  and  $K_{t2}$  in bold. Definitions of variables and their units were presented in table 2 in Elliot and Flanagan (2023).**

| No. | Soil Series            | Location          | Texture | $K_{t1}^{[a]}$ | $K_{t2}$         | $K_r$ | $\tau_c$ | Clay | Silt | Sand | FSi  | V/Sa | MSa  | Rock | OC   |
|-----|------------------------|-------------------|---------|----------------|------------------|-------|----------|------|------|------|------|------|------|------|------|
| 1   | Clarion                | Ames, IA          | FSL     | 2.03           | <b>2.37</b>      | 4.6   | 0.4      | 18.9 | 27.2 | 53.9 | 14.4 | 10.9 | 13.8 | 4    | 1.05 |
| 2   | Monona                 | Castana, IA       | SiL     | 1.78           | <b>4.76</b>      | 7.6   | 2.8      | 20.1 | 74.8 | 5.1  | 27   | 4.9  | 0    | 0    | 1.02 |
| 3   | Cecil 1 <sup>[b]</sup> | Watkinsville, GA  | SaL     | 1.18           | — <sup>[c]</sup> | 8.4   | 2.2      | 8.6  | 16.7 | 74.7 | 11.5 | 5.9  | 22.4 | 4    | 0.55 |
| 4   | Sharpsburg             | Lincoln, NE       | SiCL    | <b>1.85</b>    | <b>3.84</b>      | 5.3   | 3.2      | 39.8 | 55.4 | 4.8  | 23.9 | 4.6  | 0    | 0    | 1.85 |
| 5   | Hersh                  | Ord, NE           | SaL     | <b>3.93</b>    | <b>9.18</b>      | 11.2  | 1.7      | 9.6  | 13.4 | 77   | 2.2  | 32.9 | 18.2 | 0    | 0.49 |
| 6   | Keith                  | Albin, WY         | SiL     | <b>3.37</b>    | <b>4.07</b>      |       |          | 19.3 | 31.8 | 48.9 | 11.3 | 44   | 1    | 0    | 0.91 |
| 7   | Amarillo               | Big Spring, TX    | SaL     | <b>4.12</b>    | <b>6.78</b>      | 45.3  | 1.7      | 7.3  | 7.7  | 85   | 2.9  | 21.1 | 23.9 | 0    | 0.16 |
| 8   | Woodward               | Woodward, OK      | L       | <b>4.00</b>    | <b>10.2</b>      | 25    | 1.3      | 12.3 | 39.9 | 47.8 | 9.1  | 39   | 1.1  | 0.3  | 0.82 |
| 9   | Heiden                 | Waco, TX          | C       | <b>1.70</b>    | <b>3.23</b>      | 8.9   | 2.9      | 53.1 | 38.3 | 8.6  | 29.3 | 4.5  | 1    | 0    | 1.36 |
| 10  | Whitney                | Fresno, CA        | SaL     | <b>2.74</b>    | <b>1.83</b>      | 23.3  | 4.7      | 7.2  | 21.7 | 71.1 | 9.7  | 8.1  | 19.2 | 4    | 0.19 |
| 11  | Academy                | Fresno, CA        | SaL     | <b>2.88</b>    | <b>4.15</b>      | 5.7   | 1.6      | 8.2  | 29.1 | 62.7 | 12.2 | 20.2 | 13.7 | 4    | 0.41 |
| 12  | Los Banos              | Los Banos, CA     | SiL     | <b>2.50</b>    | <b>3.64</b>      | 0.6   | 2.1      | 43   | 41.0 | 16   | 21.1 | 11.3 | 0.8  | 0    | 1.47 |
| 13  | Portneuf               | Twin Falls, ID    | SiL     | 1.26           | <b>5.44</b>      | 10.6  | 3.1      | 11.1 | 67.4 | 21.5 | 29.4 | 19.3 | 0.5  | 0    | 0.72 |
| 14  | Nansene                | Dusty, WA         | SiL     | <b>3.12</b>    | <b>5.34</b>      | 30.7  | 3.1      | 11.1 | 68.8 | 20.1 | 30.6 | 18.1 | 0.3  | 0    | 1.49 |
| 15  | Palouse                | Pullman, WA       | SiL     | <b>4.32</b>    | <b>4.95</b>      | 6.6   | 0.7      | 20.1 | 70.1 | 9.8  | 30.9 | 8.8  | 0.1  | 0    | 1.76 |
| 16  | Zahl                   | Bainville, MT     | L       | <b>3.17</b>    | <b>5.13</b>      | 12.3  | 3.5      | 24   | 29.7 | 46.3 | 14.7 | 12.5 | 7.2  | 9    | 1.69 |
| 17  | Pierre                 | Wall, SD          | SiC     | <b>2.18</b>    | <b>3.33</b>      | 11.7  | 4.8      | 49.5 | 40.9 | 9.6  | 21.4 | 7.3  | 0.8  | 0    | 1.46 |
| 18  | Williams               | McClusky, ND      | L       | <b>2.94</b>    | <b>4.99</b>      | 4.5   | 3.4      | 26   | 32.4 | 41.6 | 17.5 | 11.5 | 8.7  | 5    | 1.79 |
| 19  | Barnes                 | Goodrich, ND      | L       | <b>1.71</b>    | <b>5.17</b>      | 3.3   | 2.3      | 24.6 | 36.0 | 39.5 | 20.6 | 12.1 | 6.7  | 4    | 3.26 |
| 20  | Sverdrup               | Wall Lake, MN     | SaL     | <b>2.11</b>    | <b>3.44</b>      | 10    | 1.4      | 7.9  | 16.8 | 75.3 | 9.4  | 3.7  | 27.3 | 0.3  | 1.28 |
| 21  | Barnes                 | Morris, MN        | L       | 1.60           | <b>4.92</b>      | 6.3   | 4        | 17   | 34.4 | 48.6 | 16.5 | 11.4 | 10.2 | 6    | 1.98 |
| 22  | Mexico                 | Columbia, MO      | SiL     | <b>2.97</b>    | <b>4.66</b>      | 3.6   | 0.7      | 26   | 68.7 | 5.3  | 33.1 | 1.1  | 1.5  | 0    | 1.56 |
| 23  | Grenada                | Como, MS          | SiL     | <b>2.63</b>    | <b>4.94</b>      | 7.3   | 4.5      | 20.2 | 77.8 | 2    | 36.4 | 1.5  | 0.2  | 0    | 1.27 |
| 24  | Tifton                 | Tifton, GA        | Sa      | <b>0.77</b>    | <b>5.28</b>      | 11.3  | 3.5      | 2.8  | 10.8 | 86.4 | 4.8  | 13.3 | 26.2 | 23   | 0.46 |
| 25  | Bonifay                | Tifton, GA        | Sa      | <b>0.87</b>    | <b>5.84</b>      | 17.9  | 1        | 3.3  | 5.5  | 91.2 | 3.1  | 16.2 | 18.6 | 1    | 0.32 |
| 26  | Cecil 2 <sup>[b]</sup> | Watkinsville, GA  | SaL     | <b>1.86</b>    | <b>3.94</b>      | 3.8   | 4.5      | 19.8 | 15.6 | 64.6 | 9.3  | 5.9  | 18.5 | 6    | 0.70 |
| 27  | Hiwassee               | Watkinsville, GA  | SaL     | 1.88           | <b>3.55</b>      | 10.3  | 2.3      | 14.7 | 21.6 | 63.7 | 15.3 | 4.3  | 19.2 | 3    | 0.83 |
| 28  | Gaston                 | Salisbury, NC     | CL      | <b>2.04</b>    | <b>4.17</b>      | 4.9   | 4.4      | 39.1 | 25.4 | 35.5 | 17.6 | 7.5  | 10.1 | 0.3  | 1.12 |
| 29  | Opequon                | Flintstone, MD    | CL      | <b>3.20</b>    | <b>3.86</b>      | 3.5   | 6.3      | 31.1 | 31.2 | 37.7 | 22.8 | 5.9  | 9.6  | 14   | 1.42 |
| 30  | Frederick              | Hancock, MD       | C       | <b>2.48</b>    | <b>5.14</b>      | 8.4   | 6.6      | 16.6 | 58.3 | 25.1 | 39.4 | 5.2  | 6.6  | 14   | 1.32 |
| 31  | Manor                  | Ellicott City, MD | L       | <b>2.69</b>    | <b>4.09</b>      | 5.4   | 3.6      | 25.7 | 30.7 | 43.6 | 23.4 | 7.1  | 10.6 | 8    | 0.96 |
| 32  | Caribou                | Presque Isle, ME  | L       | <b>1.45</b>    | <b>4.78</b>      | 4.5   | 4.3      | 12.2 | 40.8 | 47   | 25.6 | 11.5 | 7.8  | 47   | 2.28 |
| 33  | Collamer               | Ithaca, NY        | SiL     | <b>3.46</b>    | <b>5.23</b>      | 24.1  | 6.4      | 15   | 78.0 | 7    | 47.5 | 4.6  | 0.7  | 0.3  | 1.01 |
| 34  | Miamian                | Dayton, OH        | L       | <b>1.65</b>    | <b>4.36</b>      | 9.6   | 5.5      | 25.3 | 44.1 | 30.6 | 28.6 | 6.4  | 7.4  | 3    | 1.75 |
| 35  | Lewisburg              | Columbia, IN      | CL      | <b>2.47</b>    | <b>4.82</b>      | 5.9   | 3.4      | 29.3 | 32.2 | 38.5 | 19.4 | 10.9 | 7.2  | 6    | 0.87 |
| 36  | Miami                  | Waveland, IN      | SiL     | <b>1.97</b>    | <b>4.78</b>      | 9.5   | 3.3      | 23.1 | 72.7 | 4.2  | 36.9 | 2    | 0.8  | 0    | 0.82 |

<sup>[a]</sup> Units for all properties are presented in table 2 in Elliot and Flanagan (2023).

<sup>[b]</sup> “Cecil 1” was a “non-eroded” site, and “Cecil 2” was an “eroded” site, but both soils were classified as “Cecil.”

<sup>[c]</sup>  $K_{t2}$  data were not available for Cecil 1.

**Table 5c. Correlation coefficients (r) between  $K_{t1}$ ,  $K_{t2}$ ,  $K_r$ ,  $\tau_c$ , and clay content and select soil properties. Soil property descriptions and units for variables were described in table 2 in Elliot and Flanagan (2023). The soil properties with the greatest correlation coefficient for each erodibility value are highlighted.**

| Property      | $K_{t1}$      | $K_{t2}$      | $K_r$        | $\tau_c$      | Clay          | Property          | $K_{t1}$      | $K_{t2}$      | $K_r$        | $\tau_c$     | Clay   |
|---------------|---------------|---------------|--------------|---------------|---------------|-------------------|---------------|---------------|--------------|--------------|--------|
| $K_{t1}$      | <b>1.000</b>  | <b>0.390</b>  | 0.350        | -0.181        | -0.029        | N                 | <b>-0.001</b> | <b>-0.105</b> | -0.398       | 0.194        | 0.515  |
| $K_{t2}$      | <b>0.390</b>  | <b>1.000</b>  | 0.395        | -0.147        | -0.369        | Ca                | <b>0.190</b>  | <b>-0.241</b> | -0.256       | -0.042       | 0.563  |
| $K_r$         | <b>0.350</b>  | <b>0.395</b>  | 1.000        | 0.049         | -0.417        | Na                | <b>0.132</b>  | <b>-0.082</b> | 0.196        | -0.082       | 0.244  |
| $\tau_c$      | <b>-0.181</b> | <b>-0.147</b> | 0.049        | 1.000         | 0.196         | Mg                | <b>-0.091</b> | <b>-0.146</b> | -0.343       | -0.061       | 0.509  |
| Clay          | <b>-0.029</b> | <b>-0.369</b> | -0.417       | 0.196         | 1.000         | CEC               | <b>0.044</b>  | <b>-0.242</b> | -0.338       | -0.073       | 0.808  |
| Silt          | <b>0.153</b>  | <b>0.002</b>  | -0.076       | 0.209         | 0.222         | SAR               | <b>0.096</b>  | <b>-0.135</b> | 0.150        | -0.052       | 0.032  |
| Sand          | <b>-0.108</b> | <b>0.169</b>  | 0.252        | -0.256        | -0.634        | Cond              | <b>0.224</b>  | <b>-0.004</b> | -0.075       | -0.321       | 0.119  |
| V/Sa          | <b>0.400</b>  | <b>0.594</b>  | 0.249        | -0.558        | -0.327        | CaCO <sub>3</sub> | <b>-0.210</b> | <b>-0.107</b> | -0.035       | 0.002        | 0.365  |
| MSa           | <b>-0.212</b> | <b>-0.036</b> | 0.201        | -0.070        | -0.549        | Ag Stab           | <b>-0.091</b> | <b>-0.279</b> | -0.099       | 0.256        | 0.579  |
| M             | <b>0.356</b>  | <b>0.398</b>  | 0.168        | -0.083        | -0.227        | SpSf              | <b>-0.020</b> | <b>-0.324</b> | -0.391       | 0.045        | 0.899  |
| USLE-K Factor | <b>0.352</b>  | <b>0.296</b>  | 0.183        | -0.008        | -0.166        | 15Bar             | <b>-0.037</b> | <b>-0.353</b> | -0.477       | 0.174        | 0.964  |
| $K_b^{[a]}$   | <b>-0.186</b> | <b>0.294</b>  | <b>0.321</b> | <b>-0.257</b> | <b>-0.637</b> | PL                | <b>0.074</b>  | <b>0.168</b>  | -0.171       | 0.177        | 0.101  |
| Rock          | <b>-0.277</b> | <b>-0.045</b> | -0.189       | 0.314         | -0.198        | LL                | <b>0.028</b>  | <b>0.043</b>  | -0.174       | -0.061       | 0.147  |
| OC            | <b>-0.082</b> | <b>-0.131</b> | -0.408       | 0.156         | 0.437         | MC                | <b>0.217</b>  | <b>0.399</b>  | 0.118        | 0.059        | 0.029  |
| OM            | <b>0.028</b>  | <b>-0.210</b> | -0.395       | 0.186         | 0.410         | Slope             | <b>0.114</b>  | <b>0.064</b>  | -0.096       | <b>0.601</b> | 0.058  |
| WD Clay       | <b>-0.143</b> | <b>-0.341</b> | -0.350       | 0.495         | 0.698         | Order             | <b>0.518</b>  | <b>0.073</b>  | 0.054        | -0.088       | 0.025  |
| WDClay/Clay   | <b>-0.418</b> | <b>-0.193</b> | -0.002       | 0.451         | -0.183        | Miner             | <b>0.206</b>  | <b>-0.017</b> | -0.161       | -0.151       | 0.559  |
| CEC/Clay      | <b>0.124</b>  | <b>0.187</b>  | 0.091        | -0.360        | -0.161        | Miner/Clay        | <b>0.051</b>  | <b>0.416</b>  | <b>0.490</b> | -0.300       | -0.731 |
| Fe            | <b>-0.056</b> | <b>-0.274</b> | -0.355       | 0.430         | 0.426         | VSJ               | <b>-0.272</b> | <b>-0.300</b> | -0.116       | 0.075        | 0.056  |
| Al            | <b>-0.113</b> | <b>-0.200</b> | -0.373       | 0.373         | 0.291         |                   |               |               |              |              |        |

<sup>[a]</sup>  $K_b$  is the saturated hydraulic conductivity (mm h<sup>-1</sup>).

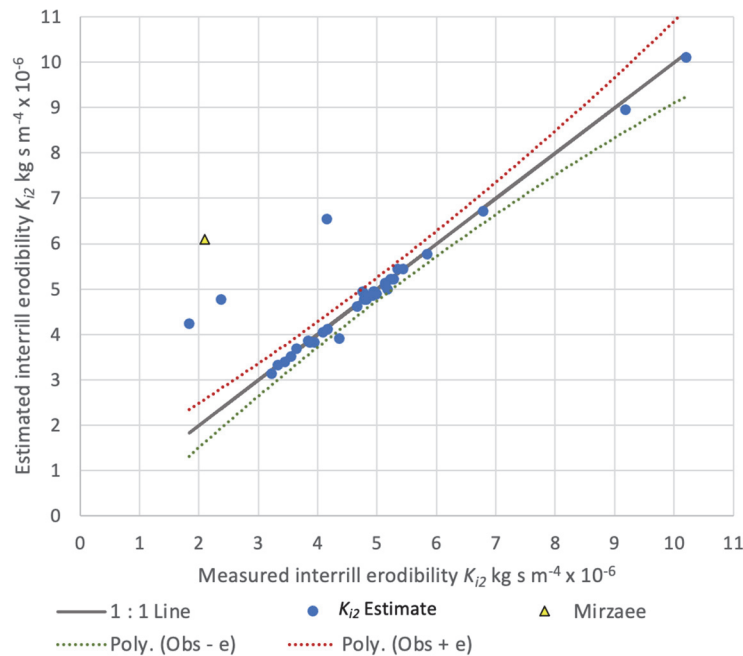


Figure 4c. Estimated interrill erodibility  $K_{12}$  from equation 12c and  $K_{12}$  confidence intervals vs. observed cropland interrill erodibility for WEPP croplands (Huffman et al., 2013) with blue dots for estimated values, red dotted line is upper confidence limit, and green dotted line is lower confidence limit ( $\alpha = 0.05$ ). Predicted vs. observed  $K_{12}$  value from Mirzaee and Ghorbani-Dashtaki (2021) is shown with a triangle. Solid line is 1:1 line. In legend, “e” is error estimate for confidence limits (Snedecor and Cochran, 1972).

## SUMMARY

We have presented a revised set of values for interrill erodibility, correcting a mistake that was made in Elliot and Flanagan (2023). The new interrill erodibility values are larger, reflecting a change in the internal WEPP interrill erosion model. The revised values confirm the validity of the predictive equations developed for interrill erodibility in Alberts et al. (1995).

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